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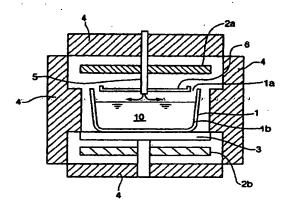
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### (54) Method for producing crystalline silicon

(57) An object of the present invention is to provide a method for producing a crystal silicon which enables to produce at a low cost and easily a polycrystalline silicon having a high quality with a low impurity content and a high crystallinity.

The method comprises the steps of: crystallizing a molten silicon from the inner bottom of a mold upward while providing to the molten silicone in the mold a temperature having a positive gradient from the inner bottom of the mold upward; and blowing, in the crystallizing step, an inert gas to the surface of the molten silicon from the upper position above the surface thereof to vibrate the surface of the molten silicon in such a manner that cavities are formed in the surface thereof.

FIG. 1



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#### BACKGROUND OF THE INVENTION

Field of the invention:

[0001] The present invention relates to a method for producing a crystalline silicon which is obtained by gradual solidification in a unidirectional way with cooling a molten silicon.

10 Description of the Related Art:

[0002] Polycrystalline silicon solar cells are solar cells which are nowadays produced in the largest quantity.

[0003] The performance of a solar cell element of polycrystalline silicon solar cell greatly depends on the quality of a polycrystalline silicon. For this reason, various improvements have been made on producing the polycrystalline silicon and the most important subjects in the production thereof are to decrease impurities in crystal and to improve crystallinity.

[0004] The production process of polycrystalline silicon is roughly divided into two steps which comprise one process for producing a high-purity silicon from a metallic silicon and the other process for solidifying a molten silicon of th high-purity silicon by a unidirectional solidification method. Conventionally, in order to decrease impurity elements, in the former method, the metallic silicon is reacted with hydrochloric acid to obtain gasfied trichlorosilane, followed by rectifying the gasfied trichlorosilane and then precipitating a high-purity silicone from the gas while reacting the rectified gas with a hydrogen gas, thereby to produce the high-purity silicone.

[0005] It is also effective that silicon is unidirectionally solidified while stirring the molten silicone such that impurity elements can be decreased.

[0006] The following methods, for examples, are disclosed for stirring. JP-A 61-141612 discloses a method of turning a mold, JP-A 5-254817 discloses a method of generating a stirring power in a molten silicon owing to a magnetic field action and JP-A 10-182135 discloses a method which comprises inserting a lance into a position above the solid-liquid phase boundary of a molten silicon and blowing an inert gas.

[0007] However, the above-mentioned first method has problems in an equipment cost, a maintenance method and a high production cost. The second method also has a problem in a high equipment cost. The third method has a problem in that the lance melts to become impurities in the molten silicon with the result of decreasing a purity of silicon.

[0008] In case of having a high oxygen content, the cell properties of a solar cell lowers. As a quantity of oxygen dissolves and is contained in a lump remelt which is a scrap of single crystal silicon used as a main raw material, it is necessary to decrease the oxygen in the process of melting and unidirectional solidification. Further, when the surface of molten silicon is not covered by an inert gas, a CO gas, SiO gas and the like enter into the molten silicon, thereby to increase the impurity content thereof and to lower the above-mentioned cell properties.

#### SUMMARY OF THE INVENTION

[0009] The present invention has been carried out, considering the above-mentioned situation. An object of the present invention is to provide a method for producing a crystalline silicon which enables to produce at a low cost and easily a polycrystalline silicon having a high quality with a low impurity content and a high crystallinity.

[0010] The following constitutions have been adopted in the present invention so as to attain the above-mentioned object:

(1) The first aspect of the present invention comprises a process for producing a crystalline silicon which crystallizes the above-mentioned molten silicon from the inner bottom of a mold upward while providing to the mold silicone in the mold a temperature having a positive gradient from the inner bottom of the mold upward, wherein an inert gas is blown to the surface of the molten silicon from the upper position above the surface thereof to vibrate the surface of the molten silicon in such a manner that cavities are formed in the surface thereof.

In the above-mentioned method for producing a crystalline silicon, an inert gas such as Ar gas is blown to the surface of the molten silicon and the surface of the molten silicon is vibrated in such a degree that the cavities are formed in the surface thereof with the result that fresh surfaces are continuously formed in the surface, thereby to promote to discharge a SiO gas generating in the interior of the molten silicon to the surrounding atmosphere and to enable to effectively remove O which is an impurity in the molten silicon.

In addition, as a gas-supplying lance is not put into the molten silicon, impurities can not enter into the molten silicon from the lance and contaminate the molten silicon.

(2) The second aspect of the present invention comprises a process for producing a crystalline silicon as men-

tioned in said (1), wherein said surface of the molten silicon is covered with an inert gas.

In the above-mentioned method for producing a crystalline silicon, as the surface of the molten silicon is covered with the inert gas such as Ar gas, impurity gases such as CO gas and SiO gas in the surrounding atmosphere are prevented from entering into the molten silicon.

(3) The third aspect of the present invention comprises a process for producing a crystalline silicon as mentioned in said any one of (1) and (2), wherein a susceptor is disposed above said surface of the molten silicon and the inert gas is introduced into a space between the susceptor and molten silicon through a part of the susceptor.

In the above-mentioned method for producing a crystalline silicon, the inert gas existing near the surface of the molten silicon is restrained from diffusing in the surrounding by the susceptor and the inert gas can cover the surface of the molten silicon for a long time. Therefore, the CO gas and SiO gas in the surrounding atmosphere are effectively prevented from entering into the molten silicon by a small flow rate of an inert gas.

(4) The fourth aspect of the present invention comprises a process for producing a crystalline silicon as mentioned in said any one of (1) to (3), wherein a flow rate of the blown inert gas is degreased according to moving of the solid-liquid phase boundary of silicon in the mold upward.

In the above-mentioned method for producing a crystalline silicon, the solid -liquid phase boundary is restrained from being disturbed by the blown inert gas.

(5) The fifth aspect of the present invention comprises a process for producing a crystalline silicon as mentioned in said any one of (1) to (4), wherein a flow rate of the blown gas, an inside radius of the gas-supplying lance which introduces the inert gas into the surface of the molten silicon and a distance from a port of the lance to the surface of the molten silicon satisfy the following formula;

 $3 \le f/(rH) \le 60$ 

where

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f [ I/min] is a flow rate of blow inert gas;

r [cm] is an inside radius of lance; and

H [cm] is a distance from a port of lance to the surface of molten silicon

In the above-mentioned method for producing a crystalline silicon, the surface of the molten silicon is vibrated under conditions selected such that a flow rate of the blown gas, an inside radius of the gas-supplying lance and a distance from a port of the lance to the surface of the molten silicon are effective and proper for promoting to discharge to the surrounding atmosphere a SiO gas which generates in the interior of the molten silicon. Therefor, O can be decreased which is an impurity in the molten silicon.

(6) The sixth aspect of the present invention comprises a process for producing a crystalline silicon as mentioned in said any one of (1) to (5), wherein the number of lance nozzles is single or plural according to the surface area of the molten silicon.

In the above-mentioned method for producing a crystalline silicon, the surface of the molten silicon is vibrated by the selected number of lance(s) according to the surface area of the molten silicon so as to be effective and proper for promoting to discharge to the surrounding atmosphere a SiO gas which generates in the interior of the molten silicon. Therefore, O can be decreased which is an impurity in the molten silicon.

#### BRIEF DESCRIPTION OF THE DRAWING

[0011]

Fig. 1 is a schematic sectional view showing the front of the mold periphery of an equipment for producing a crystalline silicone which is used in an embodiment of a method for producing a crystal silicon according to the present invention.

Fig. 2 is a plan of Fig.1 viewed from a gas-supplying lance for illustrating a gas flow.

Fig. 3 is a view showing a positional relation between a gas flow rate and a solid-liquid phase boundary.

Fig. 4 (a) is a schematic sectional view of the front of another example of a susceptor which is provided to an equipment for producing a crystalline silicone used in the embodiment of a method for producing a crystalline silicon according to the present invention.

Fig. 4 (b) is a plan of Fig.4 (a) for illustrating a gas flow.

#### Explanation of symbols:

#### [0012]

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1: mold

2a: upper heater

2b: lower heater

3: chill plate

4: thermal insulator

5: gas-supplying lance

6: susceptor

10: molten silicon

10a: solid phase

10b: liquid phase

11: solid-liquid phase boundary

#### **DESCRIPTION OF PREFERRED EMBODIMENTS**

[0013] Preferable embodiments of a method for producing a crystalline silicon in the present invention are described hereinafter with reference to drawings.

[0014] Fig.1 is a schematic sectional view showing the front of the mold periphery of an equipment for producing a crystalline silicone which is used in a method for producing a crystalline silicon according to the present invention.

[0015] In the drawing, symbols show the following:

Symbol 1 is a mold set up in a chamber which is not shown in the drawings;

Symbol 2a is an upper heater arranged above the mold;

Symbol 2b is a low heater arranged under a chill plate;

Symbol 3 is a chill plate arranged beneath the mold;

Symbol 4 is a thermal insulator surrounding the mold 1, upper heater 2a, lower heater 2b and chill plate 3;

Symbol 5 is a gas-supplying lance arranged in the upper part of the mold 1, which is inserted from the outside of the thermal insulator 4; and

Symbol 6 is a susceptor which fit the gas-supplying lance 5 in the center thereof and is arranged near an opened part 1a of the mold 1 such that the opened part 1a of the mold 1 is almost shut up.

35 [0016] First, solid silicon as a raw material is charged in the mold 1 when a crystalline silicone is produced using the above-mentioned equipment. Then, an inert gas as an atmosphere gas is introduced into the chamber from the upper part of the chamber which is not shown in the drawings and then the solid silicon in the mold is heated and melted by the upper heater 2a and lower heater 2b to make the solid silicon be a molten silicon 10. Next, an inert gas, for example, Ar gas, is supplied from the gas-supplying lance 5, to cover the surface of the molten silicon, to make such a gas flow as shown by arrow symbols in Fig.2 and to blow the gas, thereby to vibrate the surface of the molten silicon by the blown gas such that cavities are formed in the surface thereof. After that, Heating by the lower heater 2b is stopped and cooling the molten silicon in the mold by the chill plate 3 is started. In this step, the molten silicon is cooled by the chill plat starting from the bottom part 1b of the mold. The molten silicon is unidirectionally crystallized along a positive temperature gradient formed from the bottom part 1b upward.

[0017] As mentioned above, as the Ar gas is blown to the surface of the molten silicon from the upper position by the gas-supplying lance, vibration occurs in the surface and fresh faces are always formed in the surface of the molten surface. Therefore, the exhaustion of a SiO gas to the surrounding atmosphere is promoted which generates in the interior of the molten silicon with the result that O can be effectively removed which is an impurity in the molten silicon. In addition, the contamination with a CO gas from the surrounding atmosphere is prevented by this gas flow. As the solid-ification is continued in the above-mentioned state, the ingot of a crystalline silicon having a low content of impurities such as C and O is obtained after the solidification has finished. Further, a high quality of crystalline silicone having an excellent crystallinity is obtained because of having a low content of impurities according to the above-mentioned method.

[0018] Furthermore, as the opened part 1a of the mold is almost shut up by the susceptor 6 and the inert gas supplied from the gas-supplying lance covers the surface of the molten silicon, the CO gas, SiO gas and the like are prevented from entering into the molten silicon from the surface thereof.

[0019] Still furthermore, the crystalline silicon is obtained at a low cost, as it is enough if only the lance is arranged in the upper position of the mold so as to blow the inert gas to the surface of the molten silicon.

[0020] For the sake of deoxidization, it is necessary to provide a gas flow such as shown in Fig. 2 without completely closing the opened part 1a of the mold.

#### **EXAMPLES**

[0021] Ingots of crystalline silicon were produced using the above-mentioned equipment for producing a crystalline silicon according to the present invention. A mold was used which was made of quartz and had a dimension of about  $17 \times 17 \times 11$  [cm] . A 3 kg of end material which was made of a single crystal silicon for semiconductor was used as a raw material of solid silicon. Heating was carried out up to 1500°C in one hour by heaters and the melting of the raw material was finished in 1.5 hours after the heating up. The prescribed gas flow rate was set up after the melting had finished. A Ar gas was used for an atmosphere gas in the chamber

[0022] The gas-supplying lance was arranged at a location of H.= 1.0, 5.0, 12.0 and 20 [cm] which showed a height of head of the lance measured upward from the surface of the molten metal. The Ar gas was blown to the surface of the molten silicon at a flow rate of 2, 10, 40 and 60 [l/min]. The gas-supplying lances were used which had the following inside radius (r): r = 0.25, 0.5 [cm].

[0023] With regard to a gas flow rate, the rate was successively decreased according to the upward movement of the solid-liquid phase boundary. Thereby, the solid-liquid phase boundary was prevented from being disturbed with the result that a crystalline silicon having an excellent crystallinity can be produced.

[0024] As a comparative example, the following case was carried out.

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| Inside radius of gas-supplying lance: | r = 0.25 [cm]  |
|---------------------------------------|--|
| Position of lance:                    | at 300mm obliquely upward from the surface of molten silicon |
| Gas flow rate:                        | 10 [l/min]   |

[0025] The results of the impurities of thus-obtained ingots are shown in Table 1.

[0026] The height of the obtained ingots were about 5cm. With regard to both the examples of the present invention and the comparative example, C and O contents were measured in the center of the face of a wafer obtained at a height of 2.0 [cm] from the bottom of each ingot.

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| 10         |   | Comparative example   | r=0.25 | f=10     | 92.4 | The position of a port    | of lance is at 30 cm | obliquely upward from | the surface of molten | عاتد                     | r=0.25             | <b>f-</b> 10             | 2.05               | The position of a port | <b>ST</b> | obliquely upward from | the surface of molten | ailion   |
|------------|---|-----------------------|--------|----------|------|---------------------------|----------------------|-----------------------|-----------------------|--------------------------|--------------------|--------------------------|--------------------|------------------------|-----------|-----------------------|-----------------------|----------|
| 45         | , Su  |                       |        | 9        | * [  |                           |                      | <b>399</b>            | -18                   |                          |                    | 8                        | <del></del>        |                        |           |                       | 7                     |          |
| 15         | er casti  | 188                   |        | <b>4</b> | *    | 88                        |                      | 38.2                  |                       | 4 50.6                   |                    | 8                        |                    | 8                      |           |                       |                       |          |
| 20         | ngot aft  |                       | r=0.5  | 10       | 35.4 |                           |                      | 62.1                  |                       | 23.E                     | r=0.5              | 10                       |                    | <b>E</b>               | 23/4      | 1.81                  |                       | £ [      |
| 20         | iom of ii   | ntion                 |        | 2        | 45.8 | 26.2                      | 0.8                  | 85.4                  | 6                     | 90.5                     |                    | 2                        | (1.35)             | Ц                      | 1.84      | 1.97                  | 93                    | 2.04     |
| <i>2</i> 5 | the bot   | The present Invention |        | 7        | 0.1  |                           | 2.0                  | 12                    |                       | 8                        |                    | H                        | 1.0                |                        | 2.0       | 12                    |                       | 8        |
|            | an from   | The pres              |        | 09       | *    |                           | 4) [4                | (A)                   | 8                     | 39.1                     |                    | 09                       | *                  | 240                    | (Z) (A)   | <b>6:0</b>            |                       |          |
| 30         | <br>  C and O contents at 2.0 cm from the bottom of ingot after casting |                       |        | 40       | *    |                           | 77                   |                       | B                     | 97                       |                    | 40                       | *                  |                        | (S) E     |                       |                       |          |
|            | content   |                       | -0.25  | 10       | 36.5 |                           |                      | B                     |                       | 98.6                     | 1-0.25             | 21                       | 0.89               | 9                      | 21:1      | 0                     |                       | <u>8</u> |
| 35         | C and O   |                       | -      | 2        | (F)  |                           | 2.6                  | 82.1                  | F:                    | 85.0                     |                    | 2                        |                    |                        | 1.75      | 1.94                  | 6                     | 2.05     |
|            | TABLE 1   |                       |        | 1/2      | =    |                           | 5.0                  | 12                    | :                     | 20                       | 1                  | 7                        | 9                  |                        | 2.0       | 12                    |                       | 20       |
| 40         | TAB   |                       |        | (၁၁      | /wo  | 16 <sub>at</sub>          | 01×                  | )tast                 | ğαου<br>coυ           | C C                      |                    | (၁                       | 0 <b>1</b> 0       | 15 '                   | ×101      | )3mə3                 | con                   | 0        |
| 45         |   |                       |        |          |      | ) : Conditions satisfying | 3.0 ≤ f/(rH) ≤ 60    | Conditions satisfying | 5.0 ≤ f/(rH) ≤ 25     | * :Casting is impossible | as there is a high | possibility of splashing | of molten silicon. |                        |           |                       |                       |          |

[0027] In the Table 1,  $\odot$  are conditions satisfying  $5.0 \le f/(rH) \le 25$  and  $\bigcirc$  are conditions satisfying  $3.0 \le f/(rH) \le 60$ . Symbols \* are conditions wherein a molten silicon splashed and sputtered to the upper heater. The upper half of the Table shows C contents and the lower half shows O contents. The numeral which is showed in the

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fight-under of each content shows a value of f /(rH).

[0028] In cases of satisfying the conditions of 3 > f/(rH), both the C and O contens are high. In contrast, in cases of satisfying the conditions of  $3 \le f/(rH) < 5$ , the C and O contents relatively decrease. In cases of satisfying the conditions of  $5.0 \le f/(rH) \le 25$ , the C and O contents decrease approximately to a half as compared with the cases of 3 > f/(rH). In cases of satisfying the conditions of f/(rH) > 25, though the C and O contents further decrease, the crystallinity in the cell was disturbed and the cell properties lowered as it was difficult to control in such a manner that the solid-liquid phase boundary was not disturbed.

[0029] From the examples of the present invention, it is found that the C and O contents of the crystalline silicon are lower than those of the conventional example if the condition of  $3.0 \le f/(rH) \le 60$  is satisfied. Especially, in case of  $5.0 \le f/(rH) \le 25$  being satisfied, the C and O contents are greatly decreased.

[0030] In cases having a larger r, the impurity contents increase and in cases having r larger than 3 [cm], any effect is not found in decreasing the impurity contents as compared with the conventional example.

[0031] With regard to the susceptor, as shown in Fig.4, a susceptor can be used which has a larger size in a part of the diameter than the opened part of the mold and can be loaded on the opened part of the mold.

[0032] With regard to the gas-supplying lance, a plurality of lances can be used in case of a molten silicon having a large surface area.

[0033] As mentioned above in detail, the following effects are obtained according to the method for producing a crystalline silicon of the preset invention:

- (1) According to the first aspect of the present invention relating to a process for producing a crystalline silicon, a crystalline silicon can be produced which has a low impurity content and an excellent crystallinity since the solidification and crystallization are carried out while removing effectively O which is an impurity of the molten silicon by promoting to discharge a SiO gas generating in the interior of the molten silicon to the surrounding atmosphere during the crystallization.
- (2) According to the second aspect of the present invention relating to a process for producing a crystalline silicon, impurity gases such as CO gas and SiO gas in the surrounding atmosphere are prevented from entering into the molten silicon.
- (3) According to the third aspect of the present invention relating to a process for producing a crystalline silicon, a CO gas and SiO gas in the surrounding atmosphere is effectively prevented from entering into the molten silicon by a small flow rate of an inert gas.
- (4) According to the fourth aspect of the present invention relating to a process for producing a crystalline silicon, a solid-liquid phase boundary is restrained from being disturbed by a blown inert gas with the result that a crystalline silicon having an excellent crystallinty is obtained.
- (5) According to the fifth aspect of the present invention relating to a process for producing a crystalline silicon, a crystalline silicon having a greatly decreased O content can be produced since the surface of the molten silicon is effectively and properly vibrated by selecting a flow rate of the blown inert gas, an inside radius of the gas-supplying lance and a distance from a port of the lance to the surface of the molten silicon so as to promote to discharge to the surrounding atmosphere a SiO gas which generates in the interior of the molten silicon, thereby to remove O which is an impurity in the molten metal.
- (6) According to the sixth aspect of the present invention relating to a process for producing a crystalline silicon, O can be decreased which is an impurity in the molten silicon since the surface of the molten silicon is vibrated by selected number of lance(s) according to the surface area of the molten silicon so as to be effective and proper for promoting to discharge to the surrounding atmosphere a SiO gas which generates in the interior of the molten silicon.

#### Claims

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- 1. A method for producing a crystalline silicon comprising the steps of:
- crystallizing a molten silicon from the inner bottom of a mold upward while providing to the molten silicone in the mold a temperature having a positive gradient from the inner bottom of the mold upward; and blowing, in the crystallizing step, an inert gas to the surface of the molten silicon from the upper position above the surface thereof to vibrate the surface of the molten silicon in such a manner that cavities are formed in the surface thereof.
  - 2. The method for producing a crystalline silicon as claimed in claim 1, wherein said surface of the molten silicon is covered with an inert gas.

- 3. The method for producing a crystalline silicon as claimed in any one of claims 1 and 2, wherein a susceptor is disposed above said surfac of the molten silicon and the inert gas is introduced into a space between the susceptor and the molten silicon through a part of the susceptor.
- 5. 4. The method for producing a crystalline silicon as claimed in any one of claims 1 to 3, wherein a flow rate of the blown inert gas is decreased according to moving of the solid-liquid phase boundary of the silicon in the mold upward.
- 5. The method for producing a crystalline silicon as claimed in any one of claims 1 to 4, wherein a flow rate of the blown inert gas, an inside radius of a gas-supplying lance which introduces the inert gas into the surface of the molten silicon and a distance from a port of the lance to the surface of the molten silicon satisfy the following formula;

 $3 \le f/(rH) \le 60$ 

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- f [ l/min] is a flow rate of blown inert gas;
- r [ cm ] is an inside radius of lance; and
- H [ cm ] is a distance from a port of lance to the surface of molten silicon

6. The method for producing a crystalline silicon as claimed in any one of claims 1 to 5, wherein the number of lance nozzles is single or plural according to the surface area of the molten silicon.

FIG. 1

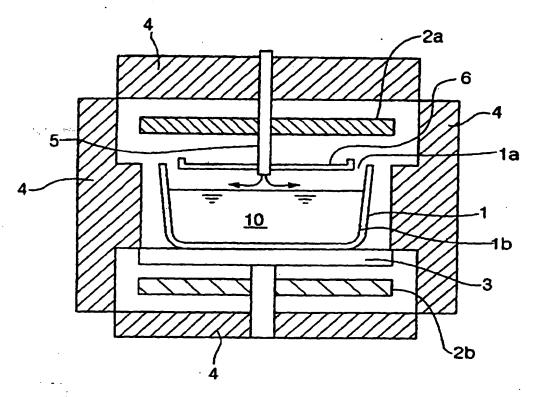


FIG 2

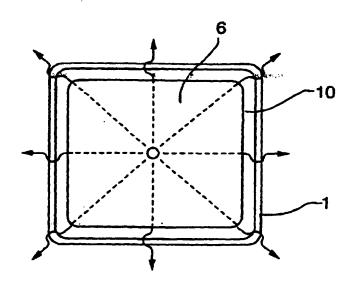
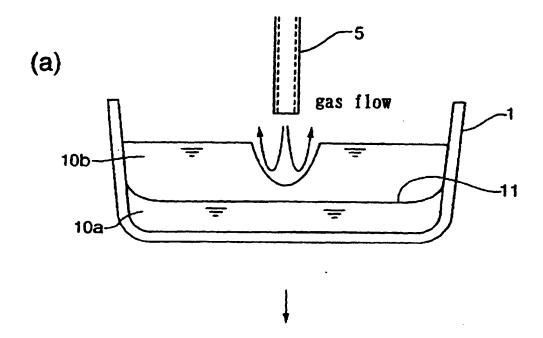


FIG. 3



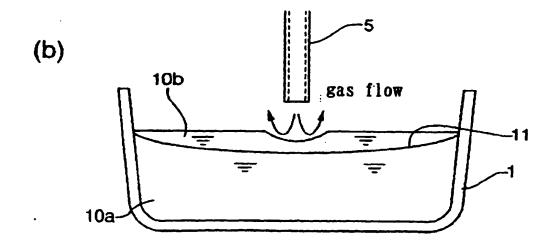
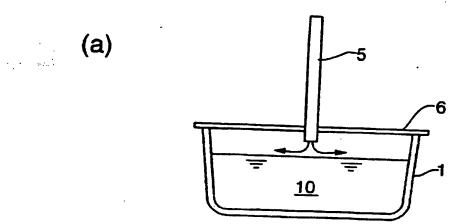
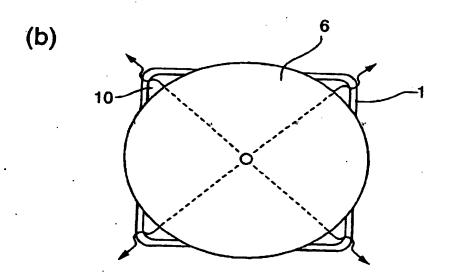


FIG. 4







# **EUROPEAN SEARCH REPORT**

EP 00 10 6163

| Category            | Citation of document with<br>of relevant pas   | indication, where appropriate,<br>sages                       | Relevant<br>to claim | CLASSIFICATION OF        |                  |
|---------------------|--|---|----------------------|--------------------------|------------------|
| X                   | EP 0 867 405 A (KA)<br>30 September 1998 (   | MASAKI STEEL CO)  | 1,2,6                | C30B11/00<br>C30B29/06   |                  |
| A,D                 | PATENT ABSTRACTS OF<br>vol. 1998, no. 12,<br>31 October 1998 (19<br>& JP 10 182135 A (19<br>7 July 1998 (1998-04<br>* abstract * | 998-10-31)<br>KAWASAKI STEEL CORP),                           |                      |                          |                  |
| A                   | WO 98 16466 A (HANA<br>STEEL CO (JP); NAKA<br>23 April 1998 (1998  | AZAWA KAZUHIRO ;KAWASAKI<br>NMURA NAOMICHI (JP);)<br>B-04-23) |                      |                          |                  |
| A                   | EP 0 887 442 A (SH/<br>30 December 1998 (1   |   |                      |                          |                  |
|                     |  |   |                      | TECHNICAL RE<br>SEARCHED | LDS<br>(Int.CL7) |
|                     |  |   |                      | C30B                     |                  |
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|                     | The present search report has  | been drawn up for all claims                                  | <del></del>          |                          |                  |
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| · C                 | ATEGORY OF CITED DOCUMENTS   | <del></del>   | underlying the i     | nvention                 | ···              |
| Y : part            | cularly relevant if taken alone<br>cularly relevant if combined with ano<br>ment of the same category                            | after the filing date   | the application      | and UI, UI               |                  |
| A : tech<br>O : non | nological beckground<br>-written disclosure<br>mediate document  | & : member of the sar   |                      | , corresponding          | ••••             |

# ANNEX TO THE EUROPEAN SEARCH REPORT ON EUROPEAN PATENT APPLICATION NO.

EP 00 10 6163

This annex lists the patent family members relating to the patent documents cited in the above-mentioned European search report. The members are as contained in the European Patent Office EDP file on The European Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

24-07-2000

| JP 10324514 A 08-12-199 JP 10324515 A 08-12-199 BR 9800953 A 28-09-199 CA 2232777 A 24-09-199 CN 1199017 A 18-11-199 NO 981311 A 25-09-199  JP 10182135 A 07-07-1998 NONE  WO 9816466 A 23-04-1998 CA 2211028 A 14-04-199 NO 974454 A 23-04-199 BR 9611816 A 13-07-199 EP 0869102 A 07-10-199 US 5961944 A 05-10-199                           | Patent document<br>cited in search repo |   | Publication date |      | Patent family member(s) | Publication date |
|--|---|---|------------------|------|-------------------------|------------------|
| JP 10324515 A 08-12-1998  BR 9800953 A 28-09-199 CA 2232777 A 24-09-199 CN 1199017 A 18-11-199 NO 981311 A 25-09-199  JP 10182135 A 07-07-1998 NONE  WO 9816466 A 23-04-1998 CA 2211028 A 14-04-199 NO 974454 A 23-04-199 BR 9611816 A 13-07-199 BR 9611816 A 13-07-199 US 5961944 A 05-10-199 EP 0887442 A 30-12-1998 JP 11011924 A 19-01-199 | EP 0867405                              | Α | 30-09-1998       | JP   | 10265214 A              | 06-10-1998       |
| BR 9800953 A 28-09-199 CA 2232777 A 24-09-199 CN 1199017 A 18-11-199 NO 981311 A 25-09-199  JP 10182135 A 07-07-1998 NONE  WO 9816466 A 23-04-1998 CA 2211028 A 14-04-199 NO 974454 A 23-04-199 BR 9611816 A 13-07-199 BR 9611816 A 13-07-199 US 5961944 A 05-10-199 EP 0887442 A 30-12-1998 JP 11011924 A 19-01-199                           |   |   |                  | JP   | 10324514 A              | 08-12-1998       |
| BR 9800953 A 28-09-199 CA 2232777 A 24-09-199 CN 1199017 A 18-11-199 NO 981311 A 25-09-199  JP 10182135 A 07-07-1998 NONE  WO 9816466 A 23-04-1998 CA 2211028 A 14-04-199 NO 974454 A 23-04-199 BR 9611816 A 13-07-199 BR 9611816 A 13-07-199 US 5961944 A 05-10-199 EP 0887442 A 30-12-1998 JP 11011924 A 19-01-199                           |   |   |                  | JP   |                         | 08-12-1998       |
| CA 2232777 A 24-09-199 CN 1199017 A 18-11-199 NO 981311 A 25-09-199  JP 10182135 A 07-07-1998 NONE  WO 9816466 A 23-04-1998 CA 2211028 A 14-04-199 NO 974454 A 23-04-199 BR 9611816 A 13-07-199 BR 9611816 A 13-07-199 US 5961944 A 05-10-199 EP 0887442 A 30-12-1998 JP 11011924 A 19-01-199  |   |   |                  | BR   |                         |                  |
| CN 1199017 A 18-11-199 NO 981311 A 25-09-199  JP 10182135 A 07-07-1998 NONE  WO 9816466 A 23-04-1998 CA 2211028 A 14-04-199 NO 974454 A 23-04-199 BR 9611816 A 13-07-199 EP 0869102 A 07-10-199 US 5961944 A 05-10-199 EP 0887442 A 30-12-1998 JP 11011924 A 19-01-199   |   |   |                  |      |                         |                  |
| NO 981311 A 25-09-199  JP 10182135 A 07-07-1998 NONE  WO 9816466 A 23-04-1998 CA 2211028 A 14-04-199   |   |   |                  | CN   |                         |                  |
| WO 9816466 A 23-04-1998 CA 2211028 A 14-04-1998  |   |   |                  |      |                         | 25-09-199        |
| NO 974454 A 23-04-199<br>BR 9611816 A 13-07-199<br>EP 0869102 A 07-10-199<br>US 5961944 A 05-10-199<br>EP 0887442 A 30-12-1998 JP 11011924 A 19-01-199   | JP 10182135                             | Α | 07-07-1998       | NONE | -                       |                  |
| BR 9611816 A 13-07-199<br>EP 0869102 A 07-10-199<br>US 5961944 A 05-10-199<br>EP 0887442 A 30-12-1998 JP 11011924 A 19-01-199  | WO 9816466                              | A | 23-04-1998       | CA   |                         | 14-04-199        |
| EP 0869102 A 07-10-199<br>US 5961944 A 05-10-199<br>EP 0887442 A 30-12-1998 JP 11011924 A 19-01-199  |   |   |                  | NO   | 974454 A                | 23-04-1998       |
| US 5961944 A 05-10-199<br>EP 0887442 A 30-12-1998 JP 11011924 A 19-01-199  |   |   |                  | BR   | 9611816 A               | 13-07-1999       |
| EP 0887442 A 30-12-1998 JP 11011924 A 19-01-199  |   |   |                  | EP   | 0869102 A               | 07-10-199        |
|  |   |   |                  | US   | 5961944 A               | 05-10-199        |
| CN 1209472 A 03-03-199   | EP 0887442                              | A | 30-12-1998       |      |                         | 19-01-199        |
|  |   |   |                  | CN   | 1209472 A               | 03-03-199        |
|  |   |   |                  |      |                         |                  |
|  |   |   |                  |      | ·                       |                  |
|  |   |   |                  |      |                         |                  |
|  |   |   |                  |      |                         |                  |
|  |   |   |                  |      |                         |                  |

For more details about this annex : see Official Journal of the European Patent Office, No. 12/82

FORM P0459